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# Design and Implement of the Front End Electronics for the CDF-II Time-of-Flight System

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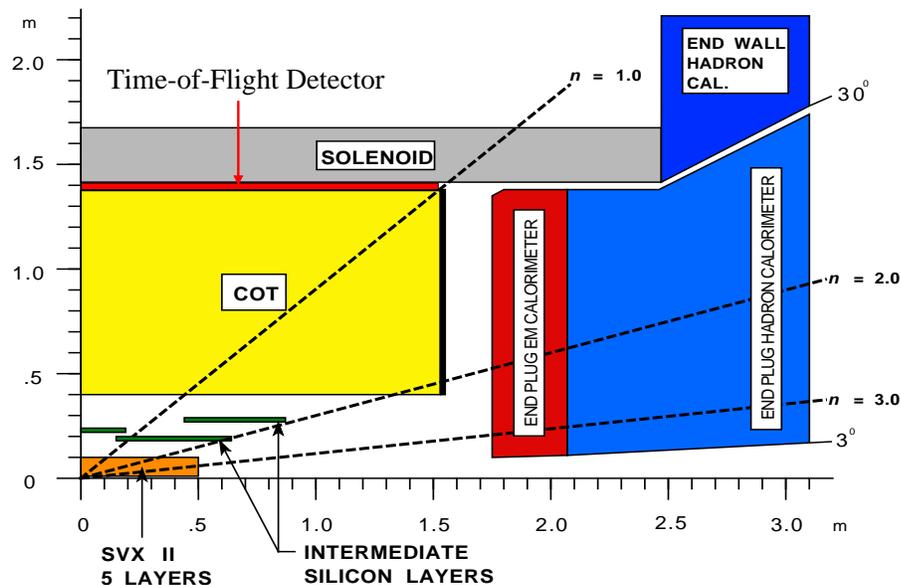
2001 IEEE NSS Conference  
8 November 2001

# TOF Development at Penn

Chunhui Chen,  
Matthew Jones,  
Walter Kononenko,  
Joseph Kroll,  
Godwin Mayers,  
Mitchell Newcomer,  
Rolf Oldeman,  
Denys Usynin,  
Richard Van Berg

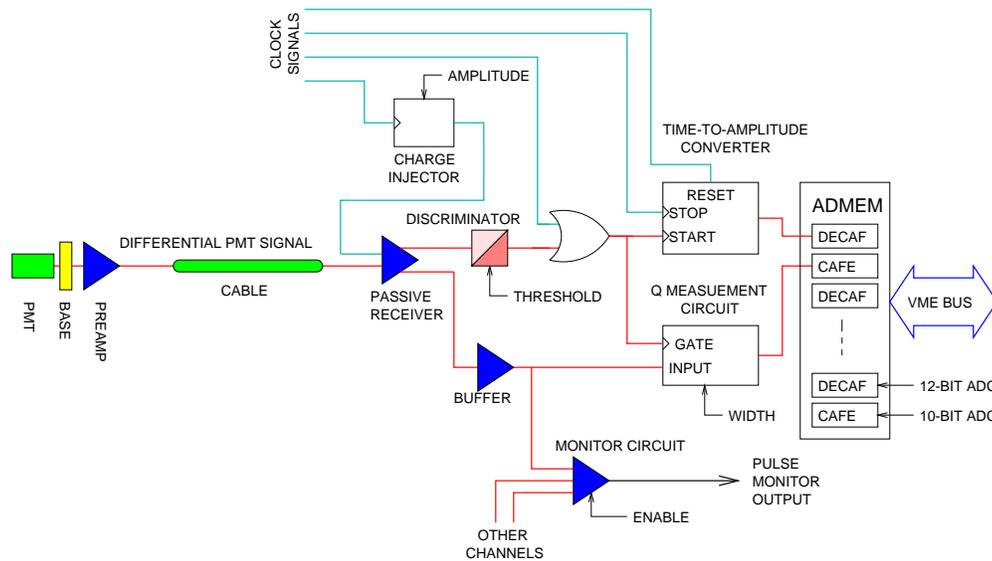
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# Overview of TOF Electronics



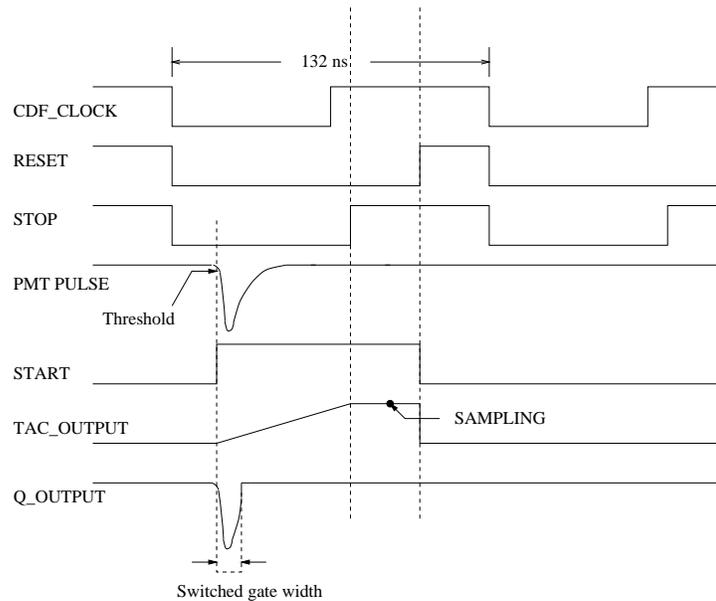
- TOF purpose: charge particle identification
- 216 Bicron BC-408 bars just outside COT
- Hamamatsu R7761 on both ends
- 432 electronics channels
- Expect time-of-flight resolution: 100 ps
- Electronics contribution: < 25 ps
- Data Acquisition rate: 7.58 MHz

# One TOF Channel



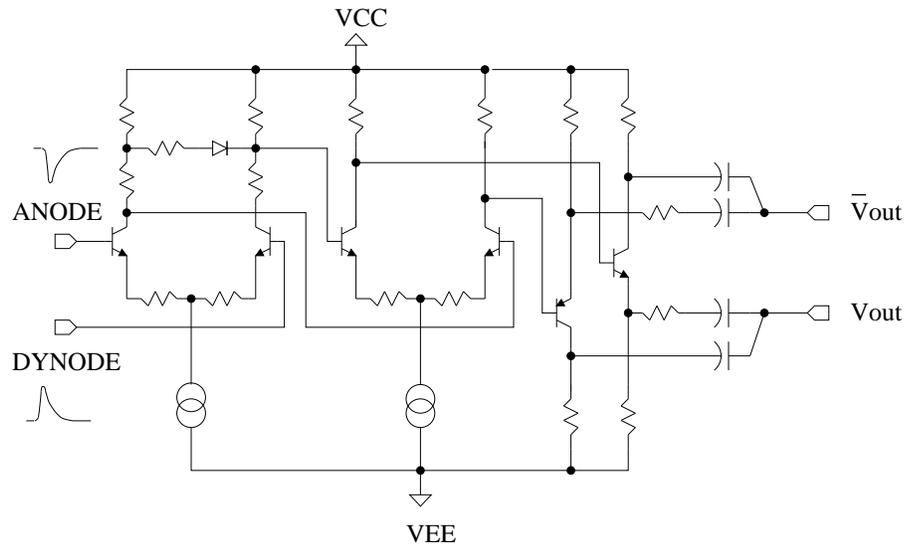
- $50 \Omega$  termination between anode and dynode
- Differential PMT output signal
- Preamplifier drives 13 m cable
- Signal path split after receiver
- Timing to amplitude converter
- Charge measurement circuit

# One TOF Channel



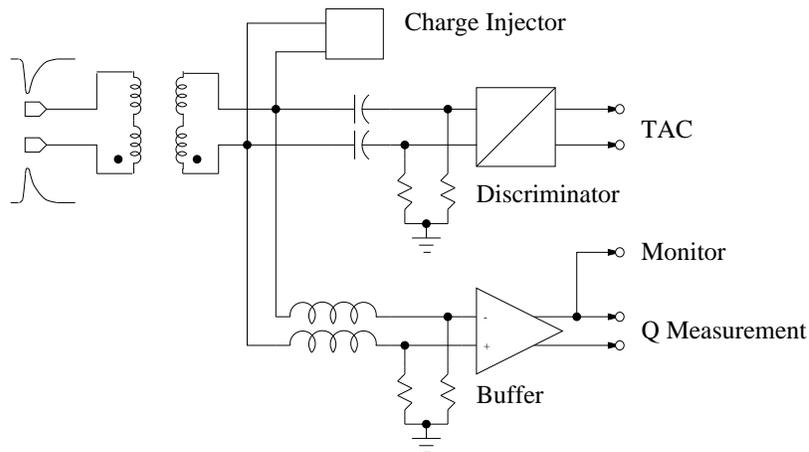
- Timing information read out by DECAF
- Charge measurement read out by CAFE
- ADMEM interface board with CDF data stream

# The Preamplifier



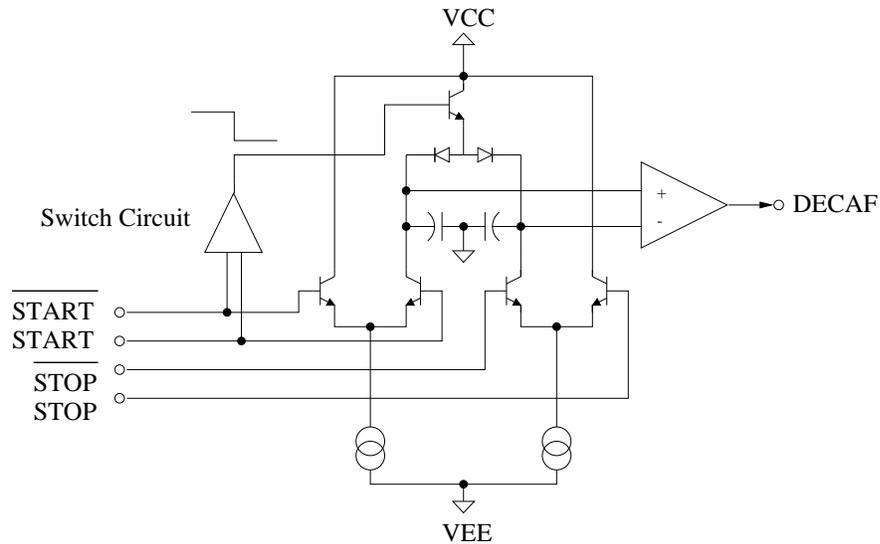
- Mounted directly behind the PMT base
- A nearly differential input from anode and last dynode
- Two differential amplifier stages and a bilinear gain
- A balanced zero-offset differential output stage with unity gain

# Receiver and Discriminator



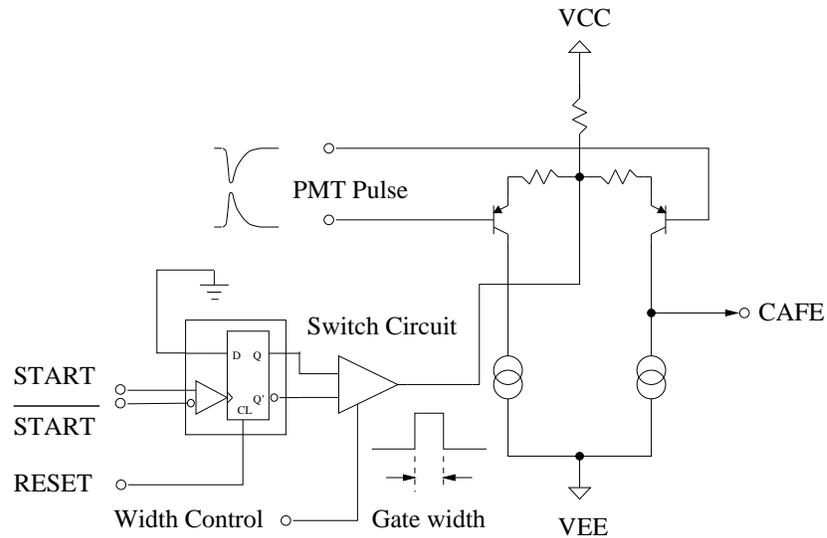
- The cable impedance matched by a parallel network
- Splits the signal into two paths
- Timing path:  
Good leading edge timing for discriminator  
Fast setting time to the baseline
- Charge path:  
A bandwidth limited version of the PMT signal  
Signal delayed to open integration gate
- Cancellation of the imaginary components of the complex termination impedance

# Time Measurement Circuit



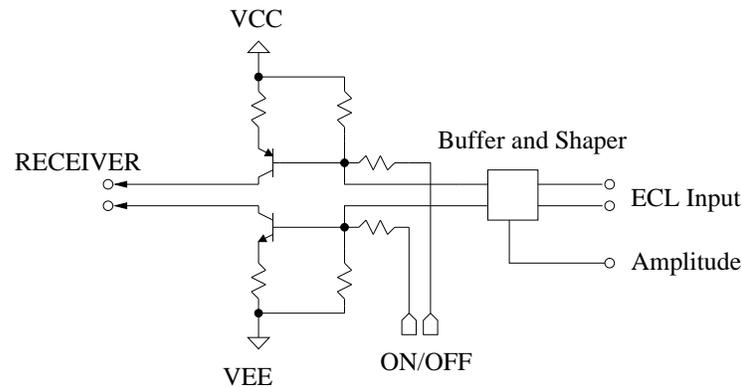
- A common stop time to amplitude converter (TAC).
- Differential ECL START signal from discriminator
- Differential ECL STOP clock signal
- High speed instrumentation amplifier output stage
- Single ended voltage output proportional to time

# Charge Measurement Circuit



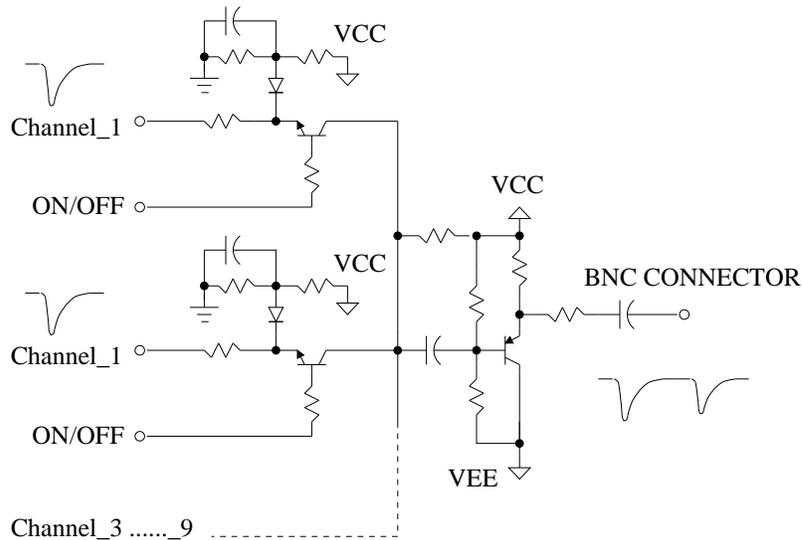
- Correct the pulse height dependence for TAC
- A trigger for highly ionizing particles
- Differential PMT input
- Single ended current output
- Initialized by the TAC START
- Switched gate with adjustable width

# Calibration

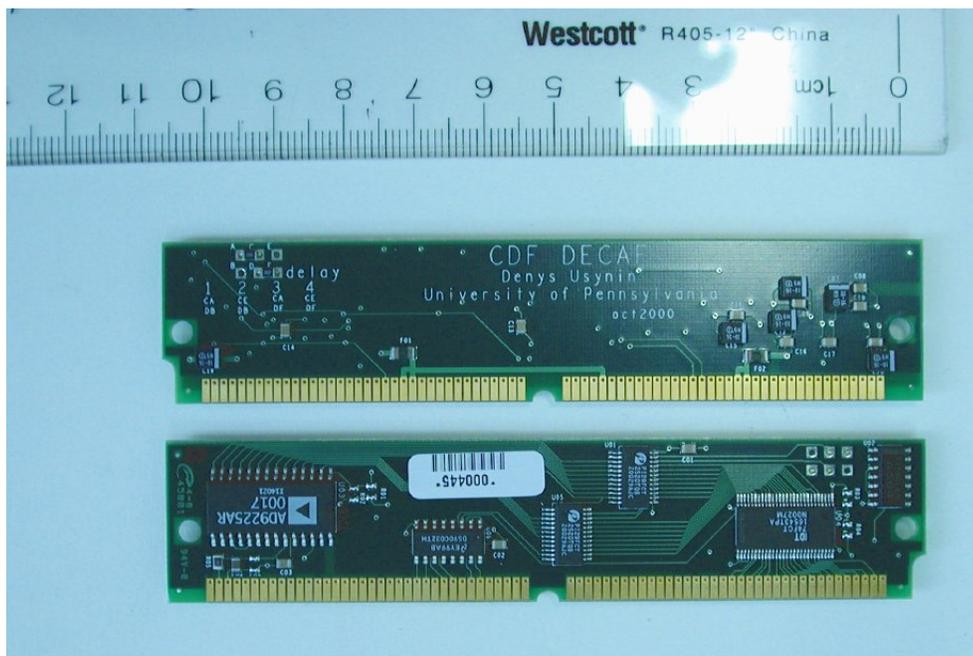
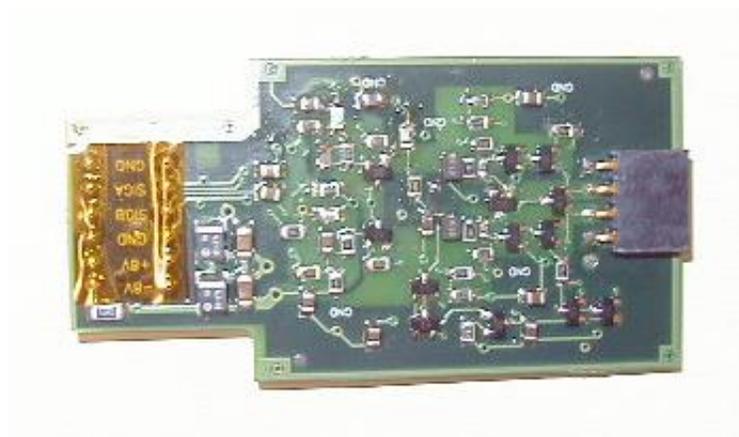


- Calibration mode 1:
  - A differential ECL calibration pulse
  - Start the TAC, bypassing the discriminator
  - Adjustable delays with respect to common stop
- Calibration mode 2:
  - Same differential ECL calibration pulse
  - A charge injector to send pulse into the receiver stage
  - Adjustable amplitude and phase

# Remote Monitoring



- A common base current summation circuit
- Monitor single or multiple PMT channels at any time
- Monitor single or multiple clock channels at any time







## Timing Performance

- Cable Delay Test:

A fixed length cable generates the common stop signal delayed with respect to a calibration pulse.

$$\text{RMS} \leq 8.5 \text{ ps}$$

$$\text{Drift} \leq 9.0 \text{ ps over } 40 \text{ hours}$$

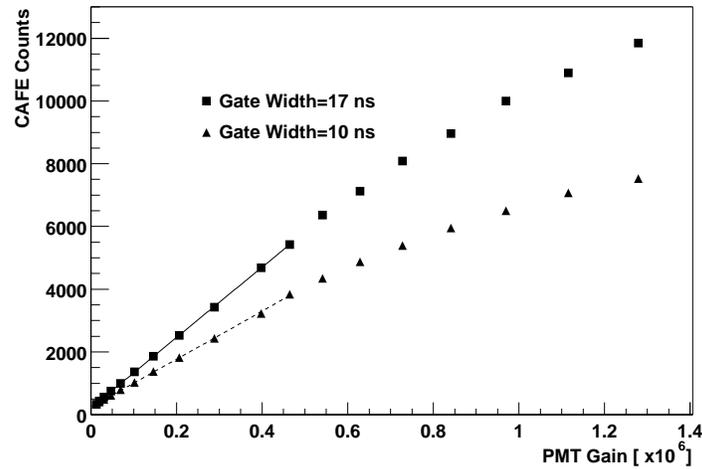
- The DDG Test:

Study the response of the TDC to a sequence of known delays generated by a DDG that has been calibrated by a digital oscilloscope.

$$V_{\text{TAC}} = \beta(1 + \gamma e^{-t/\tau})t$$

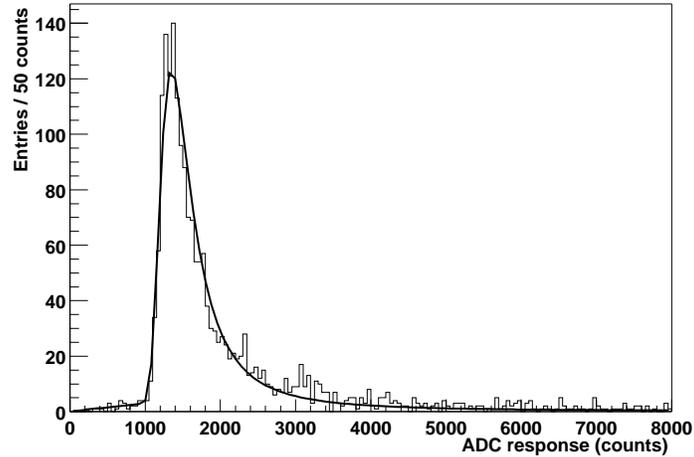
where  $\beta$ ,  $\gamma$  and  $\tau$  are parameters determined from a fit to the set of generated delays. The deviation of the measurements from the fitted curve are Gaussian distributed with a width of 5.1 ps. This parameterization adequately describes the response of all 432 channels in the system.

# Charge Measurement Performance



- Test PMT pulse generated by laser
- Adjust PMT tube HV
- Two different gate setting
- ADC response as a function of PMT gain

# Charge Measurement Performance



- ADC response due to tracks recorded at CDF
- PMT gain at  $3 \times 10^4$  in the magnetic field
- Gate width of 17 ns
- 1000 ADC counts for 1 MIP
- Larger than 12 MIP's dynamic range